

MATH 324 D, Braune

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Chapter 15

Multiple Integrals

15.1 Double Integrals over Rectangles

Recall that we approximate an integral of a function of a single variable by subdividing the region $[a, b]$ into n sub-intervals $[x_{i-1}, x_i]$ with $\Delta x = (b - a)/n$, and approximate the integral as $n \rightarrow \infty$ as:

$$\int_a^b f(x) dx = \lim_{n \rightarrow \infty} \sum_{i=1}^n f(x_i^*) \Delta x$$

We can interpret the above Riemann summation over a single variable as analogous to determining the *area* below f , where f is a positive function. Likewise, we can take Riemann integrals over *areas* to determine volume.

If we let the region R be divided into $m \times n$ sub-rectangles, and define the area of each to be $\Delta A = \Delta x \Delta y$ (where $\Delta x = (b - a)/n$, and Δy is defined analogously), then we have that:

$$V \approx f(x_{ij}^*, y_{ij}^*) \Delta A$$

and that:

$$\iint_R f(x, y) dA = \lim_{m, n \rightarrow \infty} \sum_{i=1}^m \sum_{j=1}^n f(x_{ij}^*, y_{ij}^*) \Delta A$$

The quantity above stated on either side of the equality is the volume of the surface above the region R and below the surface f .

15.1.1 Midpoint Rule

One can approximate the value of a double integral by taking a pseudo-Riemann sum evaluated only at the midpoints of each sub-region:

$$\iint_R f(x, y) dA \approx \sum_{i=1}^m \sum_{j=1}^n f(\bar{x}_{ij}, \bar{y}_{ij}) \Delta A$$

15.1.2 Average Value

Recall that we had earlier for the integral over a function of one variable that:

$$\bar{f}_{[a,b]} = \frac{1}{b-a} \int_a^b f(x) dx$$

Similarly, in the two-variable case, we have that:

$$\bar{f}_R = \frac{1}{A(R)} \iint_R f(x, y) dA$$

15.1.3 Properties of Double Integrals

Finally, note that double integrals are *linear*, meaning that they exhibit the following properties:

$$\iint_R (f(x, y) + g(x, y)) dA = \iint_R f(x, y) dA + \iint_R g(x, y) dA$$

Likewise, when c is a constant, we have that:

$$\iint_R c f(x, y) dA = c \iint_R f(x, y) dA$$

Finally, if $f \geq g$ for all $(x, y) \in R$, then:

$$\iint_R f(x, y) dA \geq \iint_R g(x, y) dA$$

15.1.4 Iterated Integrals

Consider $R = [a, b] \times [c, d]$, and observe that:

$$\iint_R f(x, y) dA = \int_a^b \left[\int_c^d f(x, y) dy \right] dx$$

When evaluating this integral, we:

- Work from the inside out, integrating f first with respect to a change in y , then with respect to a change in x .
- “Hold” the variables not being integrated as *constant* with respect to the variable currently being integrated against.

Example 15.1.1.

$$\begin{aligned} \int_0^3 \int_1^2 x^2 y dy dx &= \int_0^3 \left[x^2 \frac{y^2}{2} \right]_{y=1}^2 dx \\ &= \int_0^3 x^2 \left[\frac{2^2 - 1^2}{2} \right] dx = \frac{3}{2} \int_0^3 x^2 dx \\ &= \frac{3}{2} \left[\frac{x^3}{3} \right]_0^3 = \boxed{\frac{27}{2}} \end{aligned}$$

Note that it is often convenient to change the *order* in which a function is integrated, and that this is a legal operation due to a theorem of Fubini.

Theorem 15.1.1 (Fubini's). If f is continuous on a rectangle $R = [a, b] \times [c, d]$, then:

$$\iint_R f(x, y) dA = \int_a^b \int_c^d f(x, y) dy dx = \int_c^d \int_a^b f(x, y) dx dy$$

15.2 Double Integrals over General Regions

Call $D \subsetneq \mathbb{R}^2$ a non-rectangular region over which we would like to integrate $f(x, y)$. Then, we define:

$$F(x, y) = \begin{cases} f(x, y) & (x, y) \in D \\ 0 & \text{otherwise} \end{cases}$$

if F is integrable over R (any rectangular region enclosing D), then we have that:

$$\iint_D f(x, y) dA = \iint_R F(x, y) dA$$

- Call D a *type I* region if D is defined:

$$D = \{(x, y) : x \in [a, b], y \in [g_1(x), g_2(x)]\}$$

where it is convenient to treat the nested integral over a single x_i , thus lending a natural form:

$$\iint_D f(x, y) dA = \int_a^b \int_{g_1(x)}^{g_2(x)} f(x, y) dy dx$$

- Likewise, we call D a *type II* region if DA is defined

$$D = \{(x, y) : y \in [c, d], x \in [h_1(y), h_2(y)]\}$$

and it is likewise convenient to integrate it as

$$\iint_D f(x, y) dA = \int_c^d \int_{h_1(y)}^{h_2(y)} f(x, y) dx dy$$

- If D is more complicated, then we subdivide it into regions D_i such that each D_i is itself either a type-I or type-II region and:

$$D = \bigcup_i D_i, \quad \emptyset = D_i \cap D_j, \quad i \neq j$$

where the later statement means that any pairwise intersection of the sub-divided regions is non-overlapping. Therefore:

$$\iint_D f(x, y) dA = \sum_i \int_{D_i} f(x, y) dA$$

Note the following two properties of double integrals: first, a constant dA integrated over D is the area of that region D :

$$\iint_D dA = A(D)$$

and that if $f(x, y) \in [m, M]$ for all $(x, y) \in D$, then:

$$mA(D) \leq \iint_D f(x, y) dA \leq MA(D)$$

15.3 Double Integrals in Polar Coordinates

Recall the polar coordinate system, which often makes it easier to integrate over circular or other complicated regions. Specifically, recall that:

$$r^2 = x^2 + y^2, \quad x = r \cos \theta, \quad y = r \sin \theta, \quad \theta = \arctan(y/x)$$

a *polar rectangle* is thusly defined as:

$$R = \{(r, \theta) : r \in [a, b], \theta \in [\alpha, \beta]\}$$

and note that:

$$dA = r dr d\theta$$

15.4 Applications of Double Integrals

- To find the mass M of a planar object with density function $\rho : \mathbb{R}^2 \rightarrow \mathbb{R}$, note that:

$$M = \iint_D \rho(x, y) dA$$

- To find the average value of f in D , we have that:

$$\bar{f} = \frac{1}{A(D)} \iint_D f(x, y) dA$$

and similarly to find the weighted average (according to the corresponding density function ρ), we have:

$$\bar{f} = \frac{1}{M(D)} \iint_D \rho(x, y) f(x, y) dA$$

- We also have that, for a planar object with density ρ , that the center of mass (\bar{x}, \bar{y}) is given as:

$$\bar{x} = \frac{1}{M(D)} \iint_D x\rho(x, y) dA, \quad \bar{y} = \frac{1}{M(D)} \iint_D y\rho(x, y) dA$$

- Lastly, we can also compute the *moment of inertia* of an object spinning about some axis of rotation. Note that $\Delta m = \rho \Delta A$, and that $v = \omega r$. Then, we have that:

$$\begin{aligned} KE &= \frac{1}{2}(\Delta m)v^2 \\ &= \frac{1}{2}(\Delta m)(\omega r)^2 \\ &= \frac{1}{2}(\rho \Delta A)(\omega r)^2 = \frac{1}{2}(r^2 \rho \Delta A)\omega^2 \end{aligned}$$

and that the moment of inertia about the origin is:

$$I_0 = \iint_D r^2 \rho \, dA$$

Likewise, the moment of inertia about the x -axis is:

$$I_x = \iint_D y^2 \rho \, dA$$

and finally, about the y -axis:

$$I_y = \iint_D x^2 \rho \, dA$$

15.5 Surface Area

Let S be the surface area of a solid with equation $z = f(x, y)$, where f has continuous partial derivatives with respect to the x -, y - and z -axes.

For simplicity, we assume that $f(x, y) \geq 0$, and that the domain D is over a rectangle. We use a Riemann-like process and divide D into sub-rectangle R_{ij} , and a corresponding point $P_{ij}(x_i, y_j, f(x_i, y_j))$ where (x_i, y_j) is the point in the region closest to the origin.

Taking the summation over all tangent planes, we arrive at:

$$A(S) = \lim_{m, n \rightarrow \infty} \sum_{i=1}^m \sum_{j=1}^n \Delta T_{ij}$$

where T_{ij} is the area of the tangent plane.

We must now find the area of some ΔT for a given i, j pairing. For small enough change in x, y , this portion of the surface represents a parallelogram in 3-dimensional space. It is uniquely defined by two perpendicular curves, which at infinitesimal zoom appear as vectors, not curves. Let us call these vectors \vec{a} and \vec{b} . Note that:

$$\begin{aligned} \vec{a} &= (\Delta x, 0, f(x_0 + \Delta x, y_0) - f(x_0, y_0)) \\ &= \left(\Delta x, 0, \frac{\partial f}{\partial x}(x_0, y_0) \Delta x \right) \end{aligned}$$

$$\begin{aligned} \vec{b} &= (0, \Delta y, 0, f(x_0, y_0 + \Delta y) - f(x_0, y_0)) \\ &= \left(0, \Delta y, \frac{\partial f}{\partial y}(x_0, y_0) \Delta y \right) \end{aligned}$$

To compute the area of this parallelogram, we take the matrix determinant:

$$\begin{aligned} a \times b &\approx \begin{vmatrix} \hat{i} & \hat{j} & \hat{k} \\ \Delta x & 0 & f_x(x, y)\Delta x \\ 0 & \Delta y & f_y(x, y)\Delta y \end{vmatrix} \\ &= (-f_x\Delta x\Delta y, -f_y\Delta x\Delta y, \Delta x\Delta y) \end{aligned}$$

Then, the magnitude of $|\Delta T| = |\vec{a} \times \vec{b}|$:

$$\begin{aligned} |\Delta T| &\approx |\vec{a} \times \vec{b}| \\ &= \sqrt{f_x^2 + f_y^2 + 1} \Delta x \Delta y \end{aligned}$$

Integrating over the whole surface, we have:

$$\begin{aligned} A(S) &= \iint_R \sqrt{f_x^2 + f_y^2 + 1} dA \\ &= \iint_R \sqrt{\left(\frac{\partial z}{\partial x}\right)^2 + \left(\frac{\partial z}{\partial y}\right)^2 + 1} dA \end{aligned}$$

15.6 Triple Integrals

Whereas in the double integral case we integrated over a rectangular region (in the simple case), in the triple integral case (by contrast) we integrate over $D \subsetneq \mathbb{R}^3$. A simple case is $D = [a, b] \times [c, d] \times [e, f]$.

Again, a Riemann-like argument shows that:

$$\lim_{l, m, n \rightarrow \infty} \sum_{i=1}^l \sum_{j=1}^m \sum_{n=1}^n f(x_{ijk}^*, y_{ijk}^*, z_{ijk}^*) = \iiint_D f(x, y, z) dV$$

Note also that Fubini's theorem extends over triple integrals as well, meaning that dV can be broken down into any of the six combinations of $dx dy dz$.

We define three types of solid regions used to classify and evaluate triple integrals:

- A *type I* integral is given as $E = \{(x, y, z) : (x, y) \in D, z \in [u_1(x, y), u_2(x, y)]\}$ (that is, D is some region, and z varies between two heights.)

In this instance, it is often convenient to evaluate it as:

$$\iiint_E f(x, y, z) dV = \iint_D \left[\int_{u_1(x, y)}^{u_2(x, y)} f(x, y, z) dz \right] dA$$

- A *type II* integral is given when x varies between two constants, but y varies as a function of x , and z as a function of x and y . In this instance, it is convenient to integrate it the region as:

$$\iiint_E f(x, y, z) dV = \int_a^b \int_{g_1(x)}^{g_2(x)} \int_{u_1(x, y)}^{u_2(x, y)} f(x, y, z) dz dy dx$$

- Finally, a *type III* region is one where $(x, z) \in D$, and y varies as a function of x and z . It is typically convenient to integrate integrals of this form as:

$$\iiint_E f(x, y, z) dV = \iint_D \left[\int_{u_1(x, z)}^{u_2(x, z)} f(x, y, z) dy \right] dA$$

15.6.1 Applications of Triple Integrals

- To find the *mass* occupied by some volume, we integrate the density of that space with respect to an infinitesimal change in volume:

$$m = \iiint_R \rho(x, y, z) dV$$

- Likewise, we can find the *moments* about the three coordinate axes as follows:

$$M_{yz} = \iiint_R x\rho(x, y, z) dV \quad M_{xz} = \iiint_R y\rho(x, y, z) dV$$

$$M_{xy} = \iiint_R z\rho(x, y, z) dV$$

- The above quantities can be used to determine the center of mass, which is given as: $(\bar{x}, \bar{y}, \bar{z})$:

$$\bar{x} = \frac{M_{yz}}{m}, \quad \bar{y} = \frac{M_{xz}}{m}, \quad \bar{z} = \frac{M_{xy}}{m}$$

- Finally, if $\rho = c$ for all $(x, y, z) \in R$, then the center of mass is called the *centroid*. Likewise, the three moments of inertia about the coordinate axes are:

$$I_x = \iiint_R (y^2 + z^2)\rho(x, y, z) dV \quad I_y = \iiint_R (x^2 + z^2)\rho(x, y, z) dV$$

$$I_z = \iiint_R (x^2 + y^2)\rho(x, y, z) dV$$

15.7 Triple Integrals in Cylindrical Coordinates

In a cylindrical coordinate system, we make the following translation:

$$(x, y, z) \rightsquigarrow (r \cos \theta, r \sin \theta, z)$$

where:

$$r^2 = x^2 + y^2, \quad \tan \theta = y/x$$

Say we have a region E (of type I) which has projection D such that:

$$E = \{(x, y, z) : (x, y) \in D, z \in [u_1(x, y), u_2(x, y)]\}$$

and:

$$D = \{(r, \theta) : \theta \in [\alpha, \beta], r \in [h_1(\theta), h_2(\theta)]\}$$

We have that:

$$\iiint_E f(x, y, z) dV = \iint_D \left[\int_{u_1(x, y)}^{u_2(x, y)} f(x, y, z) dz \right] dA$$

or, converting to cylindrical coordinates, that:

$$\iiint_E f(x, y, z) dV = \int_{\alpha}^{\beta} \int_{h_1(\theta)}^{h_2(\theta)} \int_{u_1(r \cos \theta, r \sin \theta)}^{u_2(r \cos \theta, r \sin \theta)} f(r \cos \theta, r \sin \theta, z) r dz dr d\theta$$

15.8 Triple Integrals in Spherical Coordinates

Another useful coordinate system is the *spherical coordinate system*, which represents points (ρ, θ, ϕ) , where $\rho = \|\vec{P}\|_2$, θ is the same angle as in cylindrical coordinates, and ϕ is the angle between the positive z -axis and the vector \vec{P} .

Note that:

- $\rho = c$ is a sphere with radius c .
- $\theta = c$ is the half-plane with angle c about the positive x -axis.
- $\phi = c$ is a half cone which is either above or below the xy -plane, depending on whether ϕ is less than or greater than $\pi/2$, respectively.

To convert between spherical and rectangular coordinates, observe the following relationships:

$$x = \rho \sin \phi \cos \theta, \quad y = \rho \sin \phi \sin \theta, \quad z = \rho \cos \phi$$

and that:

$$\rho^2 = x^2 + y^2 + z^2$$

Our “rectangular” unit in spherical coordinates is the spherical *wedge*, which is given as:

$$E = \{(\rho, \theta, \phi) : \rho \in [a, b], \theta \in [\alpha, \beta], \phi \in [c, d]\}$$

We divide E into smaller spherical wedges, E_{ijk} , by equally spaced spheres, half-planes, and half-cones. The volume is approximately a rectangular box, with $\Delta\rho$, $\rho_i \Delta\phi$, and $\rho_i \sin \phi_k \Delta\theta$. Thus, the approximate volume of E_{ijk} is given as:

$$\begin{aligned} \Delta V_{ijk} &\approx (\Delta\rho)(\rho_i \Delta\phi)(\rho_i \sin \phi_k \Delta\theta) \\ &= \rho_i^2 \sin \phi_k \Delta\rho \Delta\theta \Delta\phi \end{aligned}$$

An application of the Mean Value Theorem yields exact equality on ΔV_{ijk} , or that:

$$\Delta V_{ijk} = \tilde{\rho}_i^2 \sin \tilde{\phi}_k \Delta\rho \Delta\theta \Delta\phi$$

where $(\tilde{\rho}_i, \tilde{\theta}_j, \tilde{\phi}_k) \in E_{ijk}$. Let $(x_{ijk}^*, y_{ijk}^*, z_{ijk}^*)$ be the rectangular coordinates of this point. Then:

$$\begin{aligned} \iiint_E f(x, y, z) dV &= \lim_{l, m, n \rightarrow \infty} \sum_{i=1}^l \sum_{j=1}^m \sum_{k=1}^n f(x_{ijk}^*, y_{ijk}^*, z_{ijk}^*) \Delta V_{ijk} \\ &= \lim_{l, m, n \rightarrow \infty} \sum_{i=1}^l \sum_{j=1}^m \sum_{k=1}^n f(\tilde{\rho}_i \sin \tilde{\phi}_k \cos \tilde{\theta}_j, \tilde{\rho}_i \sin \tilde{\phi}_k \sin \tilde{\theta}_j, \tilde{\rho}_i \cos \tilde{\phi}_k) \rho_i^2 \sin \phi_k \Delta \rho \Delta \theta \Delta \phi \end{aligned}$$

Hence,

$$\iiint_E f(x, y, z) dV = \int_c^d \int_\alpha^\beta \int_a^b f(\tilde{\rho}_i \sin \tilde{\phi}_k \cos \tilde{\theta}_j, \tilde{\rho}_i \sin \tilde{\phi}_k \sin \tilde{\theta}_j, \tilde{\rho}_i \cos \tilde{\phi}_k) \rho_i^2 \sin \phi_k d\rho d\theta d\phi$$

15.9 Change of Variables in Multiple Integrals

Recall that in single-variable calculus, we often perform a change of variable on a 1-dimensional integral as follows:

$$\int_a^b f(x) dx = \int_c^d f(g(u)) \frac{dx}{du} du$$

More generally, we consider a transformation T from the uv -plane to the xy -plane as:

$$T(u, v) = (x, y)$$

where $x = g(u, v)$, and $y = h(u, v)$ (sometimes this is written as: $x = x(u, v)$, and $y = y(u, v)$). Note that we assume T is a C^1 transformation, meaning that g and h have continuous first-order partial derivatives. Note that the inverse of these transformations are denoted $u = G(x, y)$ and $v = H(x, y)$, respectively.

Say we have the image of S (some region in uv -space) projected onto the xy -plane. Note that we can write a function for the location of the position vector in the image as follows:

$$\vec{r}(u, v) = \langle g(u, v), h(u, v) \rangle$$

Note also that we can take the tangent vectors as the first-order derivatives of \vec{r} as:

$$\vec{r}_u = \langle g_u(u_0, v_0), h_u(u_0, v_0) \rangle$$

and similarly:

$$\vec{r}_v = \langle g_v(u_0, v_0), h_v(u_0, v_0) \rangle$$

Then, we have a parallelogram whose edges are defined by \vec{a} , \vec{b} as:

$$\vec{a} = \vec{r}(u_0 + \Delta u, v_0) - \vec{r}(u_0, v_0)$$

$$\vec{b} = \vec{r}(u_0, v_0 + \Delta v) - \vec{r}(u_0, v_0)$$

But, we have that:

$$\vec{r}_u = \lim_{\Delta u \rightarrow 0} \frac{\vec{r}(u_0 + \Delta u, v_0) - \vec{r}(u_0, v_0)}{\Delta u}$$

so:

$$\vec{r}(u_0 + \Delta u, v_0) - \vec{r}(u_0, v_0) \approx \Delta u \vec{r}_u$$

and:

$$\vec{r}(u_0, v_0 + \Delta v) - \vec{r}(u_0, v_0) \approx \Delta v \vec{r}_v$$

This means that we can take the Jacobian to determine the area ΔA . The transformation *Jacobian* is given as:

$$\frac{\partial(x, y)}{\partial(u, v)} = \begin{vmatrix} \partial x / \partial u & \partial x / \partial v \\ \partial y / \partial u & \partial y / \partial v \end{vmatrix} = [(\partial x / \partial u)(\partial y / \partial v)] - [(\partial x / \partial v)(\partial y / \partial u)]$$

Thus we have (from the previous calculation):

$$\Delta A \approx \left| \frac{\partial(x, y)}{\partial(u, v)} \right| \Delta u \Delta v$$

Note that:

$$\begin{aligned} \iint_D f(x, y) dA &= \lim_{m, n \rightarrow \infty} \sum_{i=1}^m \sum_{j=1}^n f(x_i, y_j) \Delta A \\ &= \lim_{m, n \rightarrow \infty} \sum_{i=1}^m \sum_{j=1}^n f(g(u_i, v_j), h(u_i, v_j)) \left| \frac{\partial(x, y)}{\partial(u, v)} \right| \Delta u \Delta v \\ &= \iint_R f(g(u, v), h(u, v)) \left| \frac{\partial(x, y)}{\partial(u, v)} \right| du dv \end{aligned}$$

In integrals of three variables, the situation is the same. Let T be a transformation map from S in uvw -space to R in xyz -space by:

$$x = g(u, v, w), \quad y = h(u, v, w), \quad z = k(u, v, w)$$

Then, the Jacobian of T is given as:

$$\frac{\partial(x, y, z)}{\partial(u, v, w)} = \begin{vmatrix} \partial x / \partial u & \partial x / \partial v & \partial x / \partial w \\ \partial y / \partial u & \partial y / \partial v & \partial y / \partial w \\ \partial z / \partial u & \partial z / \partial v & \partial z / \partial w \end{vmatrix}$$

And thus that:

$$\iiint_R f(x, y, z) dV = \iiint_S f(x(u, v, w), y(u, v, w), z(u, v, w)) \left| \frac{\partial(x, y, z)}{\partial(u, v, w)} \right| du dv dw$$

Chapter 14

Partial Derivatives

14.5 The Chain Rule

Recall the Chain Rule for single variable functions gives that if $y = f(x)$ and $x = g(t)$, that y is indirectly differentiable by a change in t , and that:

$$\frac{dy}{dt} = \frac{dy}{dx} \frac{dx}{dt}$$

There are several such cases of the Chain Rule, each described here. First, we deal with the case where $z = f(x, y)$, and both x and y are differentiable by t . That is, if $z = f(g(t), h(t))$, then:

$$\frac{dz}{dt} = \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt}$$

In the second case, we deal with $z = f(x, y)$ where x and y are each a function of two variables, say $x = g(s, t)$, $y = h(s, t)$. Then, we have that:

$$\frac{\partial z}{\partial s} = \frac{\partial z}{\partial x} \frac{\partial x}{\partial s} + \frac{\partial z}{\partial y} \frac{\partial y}{\partial s}, \quad \frac{\partial z}{\partial t} = \frac{\partial z}{\partial x} \frac{\partial x}{\partial t} + \frac{\partial z}{\partial y} \frac{\partial y}{\partial t}$$

We now present the general case of the Chain Rule. Suppose that u is a differentiable function of x_1, x_2, \dots, x_n , and that each x_j (for $j \in [n]$) was itself differentiable by t_1, t_2, \dots, t_m . Then, u is a function of t_1, t_2, \dots, t_m , and:

$$\begin{aligned} \frac{\partial u}{\partial t_i} &= \frac{\partial u}{\partial x_1} \frac{\partial x_1}{\partial t_i} + \frac{\partial u}{\partial x_2} \frac{\partial x_2}{\partial t_i} + \dots + \frac{\partial u}{\partial x_n} \frac{\partial x_n}{\partial t_i} \\ &= \sum_{j \in [n]} \frac{\partial u}{\partial x_j} \frac{\partial x_j}{\partial t_i}, \quad \text{for } i \in [m]. \end{aligned}$$

14.6 Directional Derivatives and the Gradient Vector

Suppose now that we have a function f of two variables such that $z = f(x, y)$. We can observe the *gradient* of f , which is the vector along which z is tangent at some (x, y) , by

the following:

$$\begin{aligned}\nabla f(x, y) &= \langle f_x(x, y), f_y(x, y) \rangle \\ &= \frac{\partial f}{\partial x} \hat{i} + \frac{\partial f}{\partial y} \hat{j}\end{aligned}$$

Intuitively, ∇f gives us the direction along which f increases the fastest, whereas $|\nabla f|$ gives us the fastest rate of increase.

14.6.1 Directional Derivatives

Suppose that instead of taking the rate of change along the basis vectors in any particular subspace, that instead you wanted to compute the rate of change along some arbitrary vector \vec{u} , instead. Then, we proceed with the following derivation:

For some $u = \langle a, b \rangle$, we have that $\vec{r}(t) = \langle a_0 + at, b_0 + bt \rangle$. Then, the directional derivative is:

$$\begin{aligned}D_{\hat{u}}f(x_0, y_0) &= \lim_{h \rightarrow 0} \frac{f(x_0 + ha, y_0 + hb) - f(x_0, y_0)}{h} \\ &= \left. \frac{df(\vec{r}(t))}{dt} \right|_{t=0} \\ &= \nabla f \cdot \hat{u}\end{aligned}$$

That is, that $D_{\hat{u}}f$ is tangent to the slope along of f cut through the vertical plane containing \hat{u} . Note that:

$$D_{\hat{u}}f = \frac{df}{ds} = \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt}$$

Note that this obeys the same max/min rules as the standard dot product, and that $D_{\hat{u}}f$:

- ...is maximized when ∇f is in the direction of \hat{u} (when $\theta = 0$).
- ...is minimized under the opposite conditions (when $\theta = \pi$).
- ...is zero when $\nabla f \perp \hat{u}$ (at $\theta = \pi/2$).

Chapter 16

Vector Calculus

16.1 Vector Fields

A vector field is a space over \mathbb{R}^n whose range is \mathbb{V}_n (that is, each “point” takes on the vector of a value in the same number of dimension).

We describe such a field F as the component-wise sum of component functions P, Q , which is to say that:

$$\begin{aligned}\vec{F}(x, y) &= P(x, y)\hat{i} + Q(x, y)\hat{j} \\ &= \langle P(x, y), Q(x, y) \rangle = P\hat{i} + Q\hat{j}\end{aligned}$$

Note that we can also describe another kind of vector field over some subset of \mathbb{R}^3 ; that is the *gradient field* of some vector-valued function $\vec{f}(x, y, z)$, which is:

$$\nabla f(x, y, z) = \langle f_x(x, y, z), f_y(x, y, z), f_z(x, y, z) \rangle$$

16.2 Line Integrals

16.2.1 Parameterizations

First, say that $\vec{r} : [a, b] \rightarrow \mathbb{R}^2$ is a *parameterization* of \mathcal{C} iff $\vec{r}(t) = \langle x(t), y(t) \rangle$ is in \mathcal{C} for all $t \in [a, b]$, and that it traverses \mathcal{C} once. Some examples follow:

1. A half-circle is parameterized as follows. For $\vec{r}(t) = \langle \cos t, \sin t \rangle$, and $t \in [0, \pi]$:

$$\begin{cases} x = \cos t \\ y = \sin t \end{cases}$$

2. An ellipse of the equation $(x - 5)^2/4 + (y - 3)^2 = 1$ is parameterized for $t \in [0, 2\pi]$ as follows:

$$\begin{cases} x = 5 + 2 \cos t \\ y = 3 + \sin t \end{cases}$$

16.2.2 Line Integrals

Say that we have a curve \mathcal{C} parameterized as $\vec{r} = x(t)\hat{i} + y(t)\hat{j}$ for $t \in [a, b]$. Let us then divide the parameter into n sub-intervals of equal width as usual, and corresponding points $P_i(x_i, y_i)$ dividing \mathcal{C} into sub-arcs Δs_i for $i \in [n]$. If we let $P_i^*(x_i^*, y_i^*)$ be any point on the i th sub-arc, then the line integral of f across \mathcal{C} is:

$$\begin{aligned} \int_{\mathcal{C}} f(x, y) ds &= \lim_{\Delta s_i \rightarrow 0} \sum_{i \in [n]} f(x_i, y_i) \Delta s_i \\ &= \int_a^b f(x(t), y(t)) \sqrt{\left(\frac{dx}{dt}\right)^2 + \left(\frac{dy}{dt}\right)^2} dt \\ &= \int_a^b f(\vec{r}(t)) |\vec{r}'(t)| dt \end{aligned}$$

Example 16.2.1. Suppose that we wish to compute the area of the *fence* underneath the half-circle of radius 1 centered at the origin. Then, if $f = 2 + x^2y$, we have a parameterization:

$$\begin{cases} x = \cos t \\ y = \sin t \end{cases}$$

and that the line integral is computed as:

$$\begin{aligned} \int_{\mathcal{C}} f(x, y) ds &= \int_a^b f(\cos t, \sin t) ds \\ &= \int_a^b 2 + \cos^2 t \sin t \underbrace{\sqrt{(-\sin t)^2 + (\cos t)^2}}_1 dt \\ &= \int_a^b 2 + \cos^2 t \sin t dt = 2t - \left[\frac{1}{3} \cos^3(t) \right]_{t=0}^{\pi} \end{aligned}$$

16.2.3 Applications of Line Integrals

1. To compute the length of a line \mathcal{C} , one has:

$$\int_{\mathcal{C}} ds = \text{length}(\mathcal{C})$$

2. To compute the average value of a function f over a line \mathcal{C} , we have that:

$$\bar{f} = \frac{1}{\ell} \int_{\mathcal{C}} f ds$$

3. If $\rho(x, y)$ is the density of some function along the fence described by f and \mathcal{C} , then:

$$M = \int_{\mathcal{C}} \rho ds$$

and:

$$\bar{x} = \frac{1}{M} \int_C x \rho \, ds$$

furthermore:

$$I_y = \frac{1}{M} \int_C (x^2 + z^2) \rho \, ds$$

Note that we can use this definition to compute the *work* done by moving some particle along a path \mathcal{C} parameterized by $\vec{F} = \langle P(x, y, z), Q(x, y, z), R(x, y, z) \rangle$ by considering the i th sub-arc of \mathcal{C} and the work done to move across that:

$$\vec{F}(x_i^*, y_i^*, z_i^*) \cdot [\Delta s_i \vec{T}(t_i^*)]$$

or that the total work done is approximately:

$$\sum_{i \in [n]} [\vec{F}(x_i^*, y_i^*, z_i^*) \cdot \vec{T}(x_i^*, y_i^*, z_i^*)] \Delta s_i$$

and that:

$$\lim_{n \rightarrow \infty} \sum_{i \in [n]} [\vec{F}(x_i^*, y_i^*, z_i^*) \cdot \vec{T}(x_i^*, y_i^*, z_i^*)] \Delta s_i = \int_C \vec{F} \cdot \vec{T} \, ds$$

where $\vec{T} = \frac{\vec{r}'(t)}{|\vec{r}'(t)|}$.

16.3 The Fundamental Theorem for Line Integrals

Before discussing the Fundamental Theorem for Line Integrals, let us first discuss a couple of kinds of line integrals:

1. If we have that $F = \langle P, Q \rangle$ (or, alternatively, that $F = \langle P, Q, R \rangle$ if we are in \mathbb{R}^3), then we can write that:

$$\begin{aligned} \int_C \vec{F} \cdot d\vec{r} &= \int_C \langle P, Q, R \rangle \cdot \langle dx, dy, dz \rangle \\ &= \int_C P \, dx + Q \, dy + R \, dz \end{aligned}$$

where P , Q , and R take $\mathbb{R}^3 \rightarrow \mathbb{R}$ (i.e., that they are a function of (x, y, z)), and that dx , dy , and dz are the residual differentials (when with respect to time) of a parameterization of \mathcal{C} .

Alternatively, we can write this same kind of integral as:

$$\int_C \vec{F} \cdot d\vec{r} = \int_{r(t) \in \mathcal{C}} \vec{F}(\vec{r}(t)) \cdot \frac{d\vec{r}}{dt} \, dt$$

2. Secondly, we discuss line integrals over vector fields:

$$\begin{aligned}\int_{\mathcal{C}} \nabla f \cdot d\vec{r} &= \int_{\vec{r}(t) \in \mathcal{C}} \frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt} + \frac{\partial f}{\partial z} \frac{dz}{dt} \\ &= \int_{\vec{r}(t) \in \mathcal{C}} \left[\frac{d}{dt} f(\vec{r}(t)) \right] dt\end{aligned}$$

Theorem 16.3.1. Let \mathcal{C} be a smooth curve parameterized by $\vec{r}(t)$ for $t \in [a, b]$. Let f be a differentiable function of two or three variables, whose gradient vector ∇f is continuous on \mathcal{C} . Then:

$$\int_{\mathcal{C}} \nabla f \cdot d\vec{r} = f(\vec{r}(b)) - f(\vec{r}(a)).$$

Proof.

$$\begin{aligned}\int_{\mathcal{C}} \nabla f \cdot d\vec{r} &= \int_a^b \nabla f(\vec{r}(t)) \cdot \vec{r}'(t) dt \\ &= \int_a^b \left(\frac{\partial f}{\partial x} \frac{dx}{dt} + \frac{\partial f}{\partial y} \frac{dy}{dt} + \frac{\partial f}{\partial z} \frac{dz}{dt} \right) dt \\ &= \int_a^b \frac{d}{dt} f(\vec{r}(t)) dt \\ &= f(\vec{r}(b)) - f(\vec{r}(a)).\end{aligned}$$

□

Note that this implies the following three equivalent properties:

1. \vec{F} is path-independent (i.e., that if any other paths have the same endpoints that they integrate the same work).
2. \vec{F} is conservative (i.e., that if \mathcal{C} is a closed loop that $\int_{\mathcal{C}} \vec{F} \cdot d\vec{r} = 0$).
3. \vec{F} is a gradient field (i.e., that $\vec{F} = \nabla f$).

One way to visualize that (1) \iff (2) is that one can form a closed loop \mathcal{C} as $\mathcal{C} = \mathcal{C}_1 - \mathcal{C}_2$ where \mathcal{C}_1 and \mathcal{C}_2 have the same endpoints and flow in the same direction. Note that this implies path-independence from a conservative path (i.e., that \mathcal{C} is conservative).

16.3.1 Tests for Gradient Fields

Note that it is often important to test whether a field is indeed that of a gradient field for some function f . One way to test this in two dimensions is as follows:

Say that $\vec{F} = \langle P, Q \rangle = \nabla f$. Then, we have that:

$$P = \frac{\partial f}{\partial x} = f_x, \quad \text{and} \quad Q = \frac{\partial f}{\partial y} = f_y$$

therefore, if we consider P_y and Q_x , it is clear that $f_{xy} = f_{yx}$ and that this must be a gradient field. Note that F must be defined at every point in the plane for this to be the case (i.e., the gradient ∇f must be defined everywhere).

Another example follows for the three-dimensional case. Let $\vec{F} = \langle P, Q, R \rangle$. If $\vec{F} = \nabla f$, then:

$$\begin{aligned} P_y &= f_{xy} = f_{yx} = Q_x \\ Q_z &= f_{yz} = f_{zy} = R_y \\ R_x &= f_{xz} = f_{zx} = P_z \end{aligned}$$

Theorem 16.3.2. If $\vec{F} = \langle P, Q, R \rangle$ is defined for all $(x, y, z) \in \mathbb{R}^3$, and $P_y = Q_x$, $Q_z = R_y$, and $R_x = P_z$, then there exists some f for which $\vec{F} = \nabla f$.

Example 16.3.1. Suppose that we have:

$$\begin{aligned} f_x &= y^2 \\ f_y &= 2xy + e^{3z} \\ f_z &= 3ye^{3z} \end{aligned}$$

Then we have that $\int f_x dx = f = xy^2 + g(y, z)$, which we can differentiate to obtain $f_y = 2xy + g_y(y, z)$, which we know from the given is equal to $2xy + e^{3z}$, implying that $g_y(y, z) = e^{3z}$. Then we have that $g(y, z) = ye^{3z} + h(z)$, so that $f = xy^2 + ye^{3z} + h(z)$, and that after a similar such computation that $h = K$.

So, we conclude that:

$$f(x, y, z) = xy^2 + ye^{3z} + K$$

and that we are in a vector field, or equivalently that $\nabla f = \vec{F}$.

16.4 Green's Theorem

Theorem 16.4.1 (Green's).

$$\oint_{\mathcal{C}} P dx + Q dy = \iint_D \left(\frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y} \right) dA$$

We use $\oint_{\mathcal{C}}$ to indicate that \mathcal{C} is a bounded line with positive orientation.

Consider the following example:

Example 16.4.1. Say we wish to integrate the work done by $\vec{F} = \langle 3y - e^{\sin x}, 7x + \sqrt{y^4 + 1} \rangle$ along the path \mathcal{C} described by the positively-oriented rotation about the origin of $r^2 = 9$.

Then:

$$\begin{aligned}
 \oint_{\mathcal{C}} \vec{F} \cdot d\vec{r} &= \oint_{\mathcal{C}} (3y - e^{\sin x}) dx + (7x + \sqrt{y^4 + 1}) dy \\
 &= \iint_D \left(\frac{\partial}{\partial x} [7x + \sqrt{y^4 + 1}] - \frac{\partial}{\partial y} [3y - e^{\sin x}] \right) dA \\
 &= \int_0^{2\pi} \int_0^3 (7 - 3) r dr d\theta \\
 &= 36\pi
 \end{aligned}$$

Note that for Green's Theorem to be applicable, we must have that the curve \mathcal{C} is *closed*, i.e., that it has no "endpoint". Likewise, we must have that the curve is *positively oriented*, meaning that the region D is bounded by the left-hand side of the curve when travelling along it.

16.4.1 Criterion for Gradient Fields

Note also that when applying Green's theorem, if $\vec{F} = \nabla f$, then any closed line integral will equal 0. This is trivial from the fact that $\vec{F} = \nabla f \implies Q_x = P_y$, and:

$$\begin{aligned}
 \oint_{\mathcal{C}} \vec{F} \cdot d\vec{r} &= \oint_{\mathcal{C}} P dx + Q dy \\
 &= \iint_D (Q_x - P_y) dA = 0
 \end{aligned}$$

16.4.2 Green's Theorem for Area

To find the area enclosed by a positively oriented \mathcal{C} , we can choose a field $\vec{F} = \langle P, Q \rangle$ such that $Q_x - P_y = 1$, and then we have that:

$$\oint_{\mathcal{C}} P dx + Q dy = \iint_D 1 dA$$

16.5 Curl and Divergence

For a vector field $\vec{F} = \langle P, Q \rangle \in \mathbb{R}^2$, we have:

$$\text{curl}(\vec{F}) = \frac{\partial Q}{\partial x} - \frac{\partial P}{\partial y}$$

and

$$\text{div}(\vec{F}) = \frac{\partial P}{\partial x} + \frac{\partial Q}{\partial y}$$

16.5.1 Green's Theorem (vector version)

Consider a line \mathcal{C} such that $\mathcal{C} = \partial D$, with $r(t) = (x(t), y(t))$ for $t \in [a, b]$. Note the following special vectors:

- Unit tangent vector:

$$\vec{T} = \frac{(x', y')}{\sqrt{(x')^2 + (y')^2}}$$

- Outward unit normal:

$$\vec{N} = \frac{(x', -y')}{\sqrt{(x')^2 + (y')^2}}$$

- Length element:

$$ds = \sqrt{(x')^2 + (y')^2}$$

Then we have that:

$$\oint_{\mathcal{C}} \vec{F} \cdot \vec{T} ds = \iint_D \text{curl}(\vec{F}) dA$$

is the *circulation* of \vec{F} around \mathcal{C} . Likewise, we have that:

$$\oint_{\mathcal{C}} \vec{F} \cdot \vec{N} ds = \iint_D \text{div}(\vec{F}) dA$$

is the *flux* of \vec{F} through \mathcal{C} .